

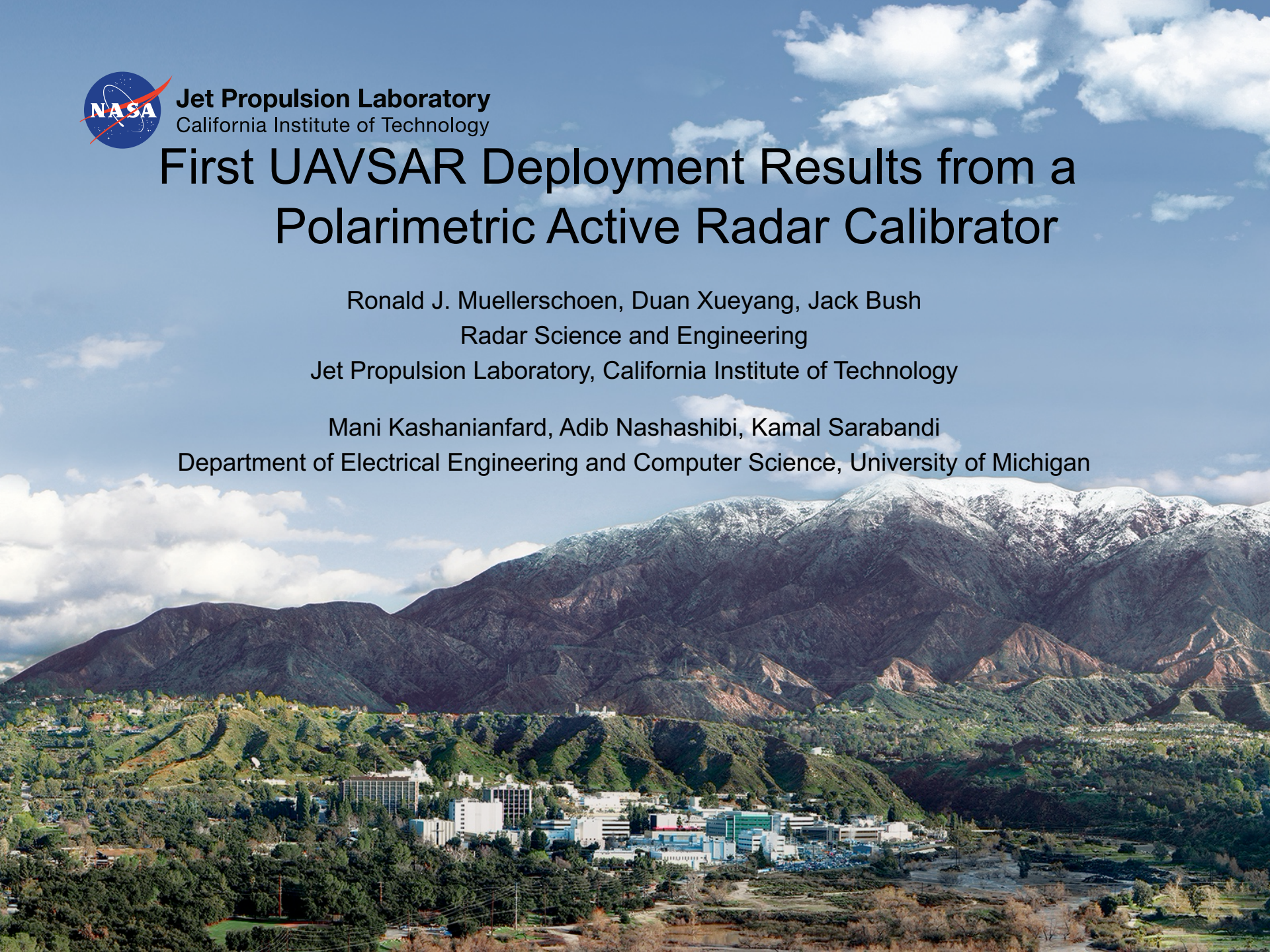
Jet Propulsion Laboratory
California Institute of Technology

First UAVSAR Deployment Results from a Polarimetric Active Radar Calibrator

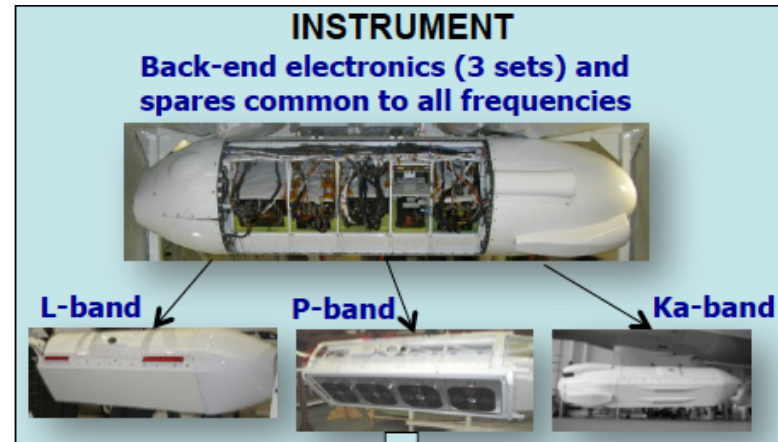
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UAVSAR Airborne Instrument



	P-band/UHF	L-band	Ka-band
Frequency (MHz)	280 – 440	1217.5-1297.5	35,620-35,700
Nominal Bandwidth (MHz)	20	80	80
Selectable Bandwidths (MHz)	6, 20, 40, 80	80	80
Polarization	Quad-pol	Quad-pol	Horizontal
Peak Transmit Power (kW)	2.0	3.1	0.08
Maximum Duty Cycle	10%	8%	10%
Look Angle Range	25 – 50 deg	25-65 deg	15-50
Nominal Range Swath (km)	9	22	10
Noise Equivalent Sigma0 (dB)	< -40	< -50	TBD
Radiometric Accuracy (dB)	< 1 absolute	< 1 absolute	TBD
Height Precision (30x30 m posting)	N/A	N/A	0.1 – 0.5 m

Rosamond Corner Reflector Array

UAVSAR 80 MHz Polarmetric L-band Image Sept, 2017



- 5 4.8 meter corners – all with 350 degree azimuth heading
- 23 2.4 meter corners – 10 with 350 heading, 13 with 170 heading
- 10 0.7 meter corners – 4 with 350 heading, 6 with 90 heading

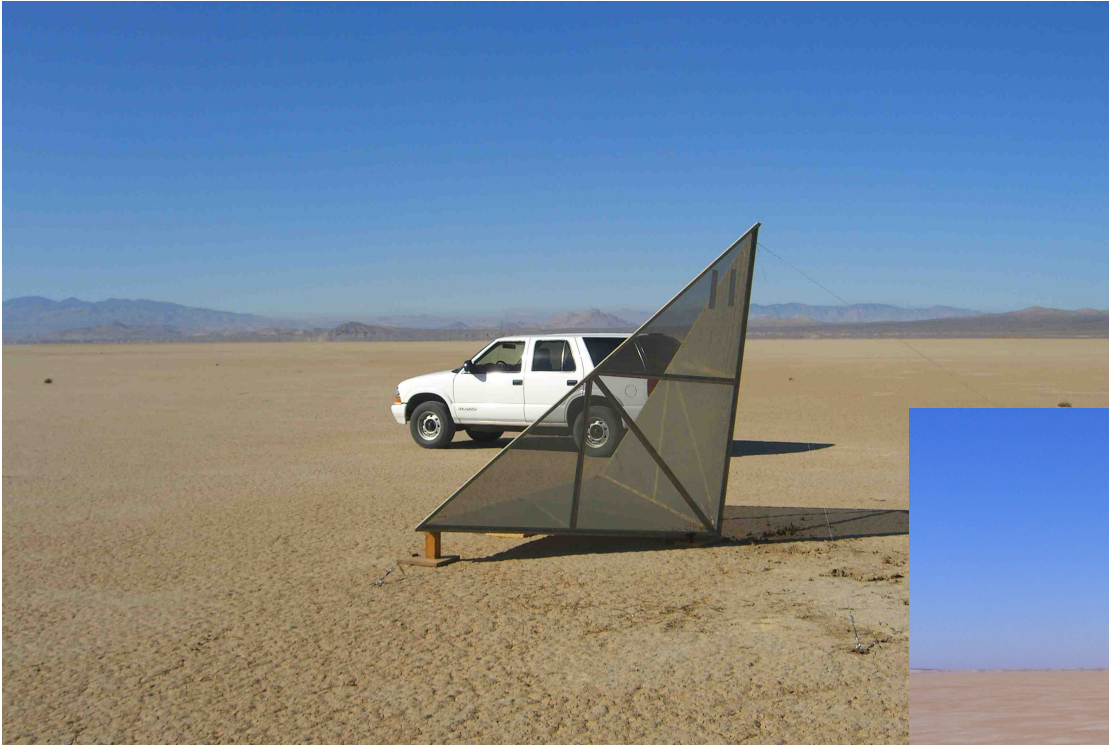
0.7 Meter Trihedral Corner Reflector for Ka-band

4 at 350 heading (installed Dec, 2015), 6 at 90 heading (installed June, 2018)



2.4-meter Trihedral Corner Reflector for L-band

10 at 350 heading, 13 at 170 heading

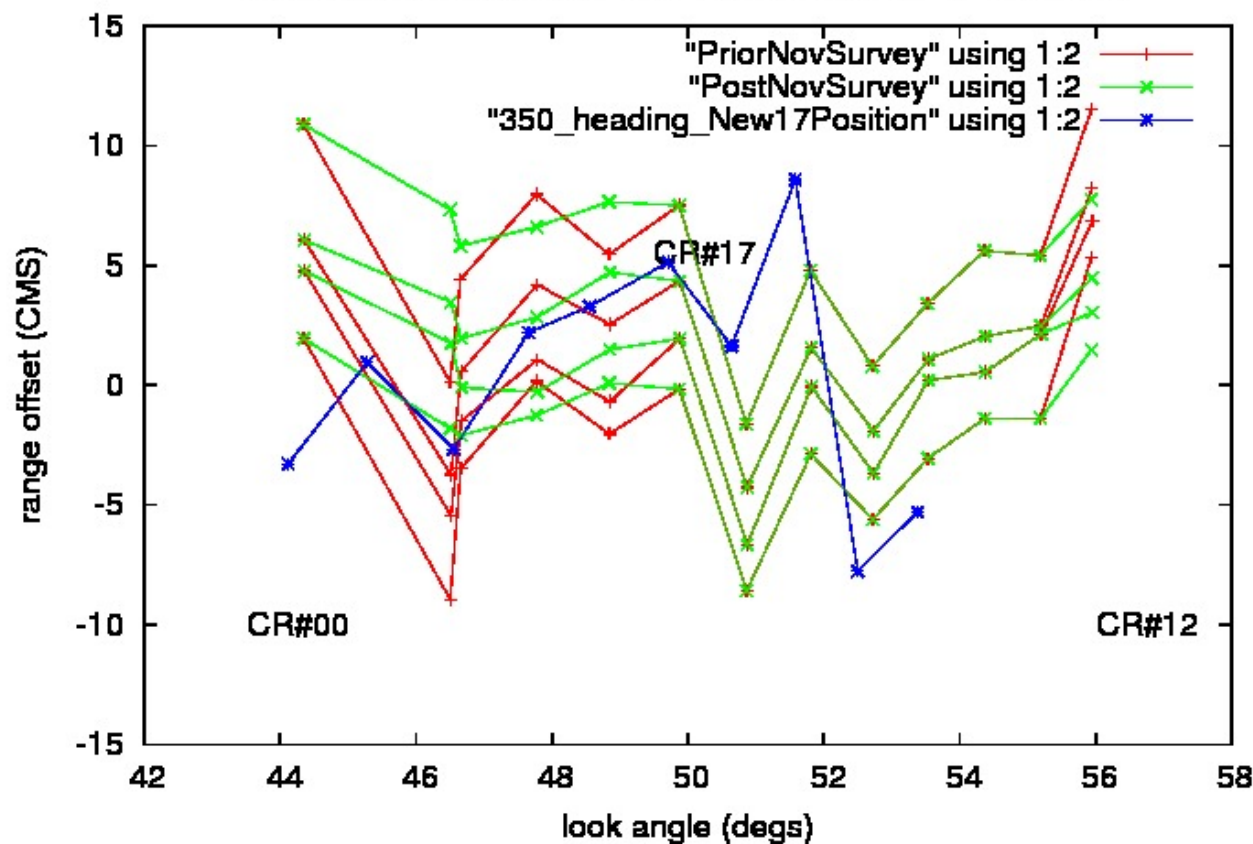


2.4-meter Trihedral Corner Reflector for L-band

CR#01, #02, #03, #04, #12 resurveyed Nov 1st, 2018

CR#17 repositioned Nov 7th, 2018

UAVSAR RCRA Passes 2018aug14, 2018sep14, 2018nov27



CR#17 moved
16 meters West
6 meters North

Need to resurvey
CR#00, CR#06,
CR#07, CR#08 then
all the 170 heading
CRs should then have
a range accuracy of
better than 1.2 CMS
RMS.

<https://uavsar.jpl.nasa.gov/cgi-bin/calibration.pl>

4.8 meter Trihedral for P-band (and L-band)

5 at 350 heading (installed May, 2012)



Single Antenna Polarimetric Active Radar Calibrator



Single Antenna PARC

- Receives/Transmits through a single antenna with a dual-polarized horn.
- Uses an orthomode transducer (OMT) that provides 60 dB isolation between dual-pole transmitting and receiving polarizations.
- Reduces signal leakage within the antenna with passive leakage cancelation circuitry.
- Achieves an active gain by monitoring a reference signal generated by temperature regulated voltage controlled crystal oscillator (VCXO).
- Has an equal magnitude scattering matrix response due to 45 degree rotation in plane perpendicular to direction of incidence.

$$S_{PARC} = \begin{pmatrix} S_{HH} & S_{HV} \\ S_{VH} & S_{VV} \end{pmatrix} = \begin{pmatrix} 1 & 1 \\ -1 & -1 \end{pmatrix} \quad S_{Trihedral} = \sqrt{\sigma_{cr}} \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$$

$$\phi_{HH-VV} = \phi_{HV-VH} = \pi$$

$$\phi_{HH-VV} = 0$$

$$\phi_{HH-HV} = \phi_{VH-VV} = 0$$

Sarabandi, K., Oh, Y., Ulaby, F., "Performance Characterization of Polarimetric Active Radar Calibrators and a New Single Antenna Design," in IEEE Transactions On Antennas and Propagation, Vol. 40, No. 10, October 1992.

- Can evaluate cross-pol response, which cannot be estimated by passive trihedral targets.
- Provides direct computation of the cross-pol channel imbalance.

Single Antenna PARC

- High signal-to-clutter ratio.
 - To reduce calibration errors.
 - Has a configurable RCS value from 40 dBsm to 55 dBsm.
 - 55 dBsm @ L-band ~ to a 8.1 meter Trihedral CR with a 11.5 meter leading edge
- Can be deployed for remote operation.
 - Has a self contained on-board processor, receiver and digitizer.
 - Contains communication equipment for data storage and download.
 - Is solar powered, with rechargeable 24 Volt, 100 Ah Lithium Battery.
 - Has thermoelectric cooling to extend its application to high temp environment.
- Mature and sophisticated tools for remote programmability
 - WEB based scheduling for satellite passes.
 - SMS (cell phone) interface for instantaneous elevation and RCS settings.
 - Hand-held controller which accommodates a SAR indicator light.
 - New mobile device app available.
 - Hosts self diagnostics.
 - Logs engineering data to WEB.

NISAR and UAVSAR Clutter Statistics

Assuming -5 dBsm clutter background*

NISAR/UAVSAR clutter characteristics												
		<u>NISAR</u>										<u>UAVSAR</u>
Mode #		10	20	30	40	50	60	54	43	63	56	
Range Bandwidth	MHz	25	80	5	25	45	45	45	25	45	45	80
Ground Range Res. (n)	m	13.44	3.35	53.77	13.44	6.72	6.72	6.72	13.44	6.72	6.72	
Ground Range Res. (f)	m	10.21	2.84	40.86	10.21	5.11	5.11	5.11	10.21	5.11	5.11	1.67
Azimuth Resolution	m	6.05	6.05	6.05	6.05	6.05	6.05	6.05	6.05	6.05	6.05	0.8
Ground pixel size (n)	m ²	81.3	20.3	325.3	81.3	40.7	40.7	40.7	81.3	40.7	40.7	
Ground pixel size (f)	m ²	61.8	17.2	247.2	61.8	30.9	30.9	30.9	61.8	30.9	30.9	1.34
Ave. Clutter RCS (n)	dBsm	14.1	8.1	20.1	14.1	11.1	11.1	11.1	14.1	11.1	11.1	
Ave. Clutter RCS (f)	dBsm	12.9	7.4	18.9	12.9	9.9	9.9	9.9	12.9	9.9	9.9	-3.7

*Rosamond Dry Lake Bed clutter background is < -30 dBsm

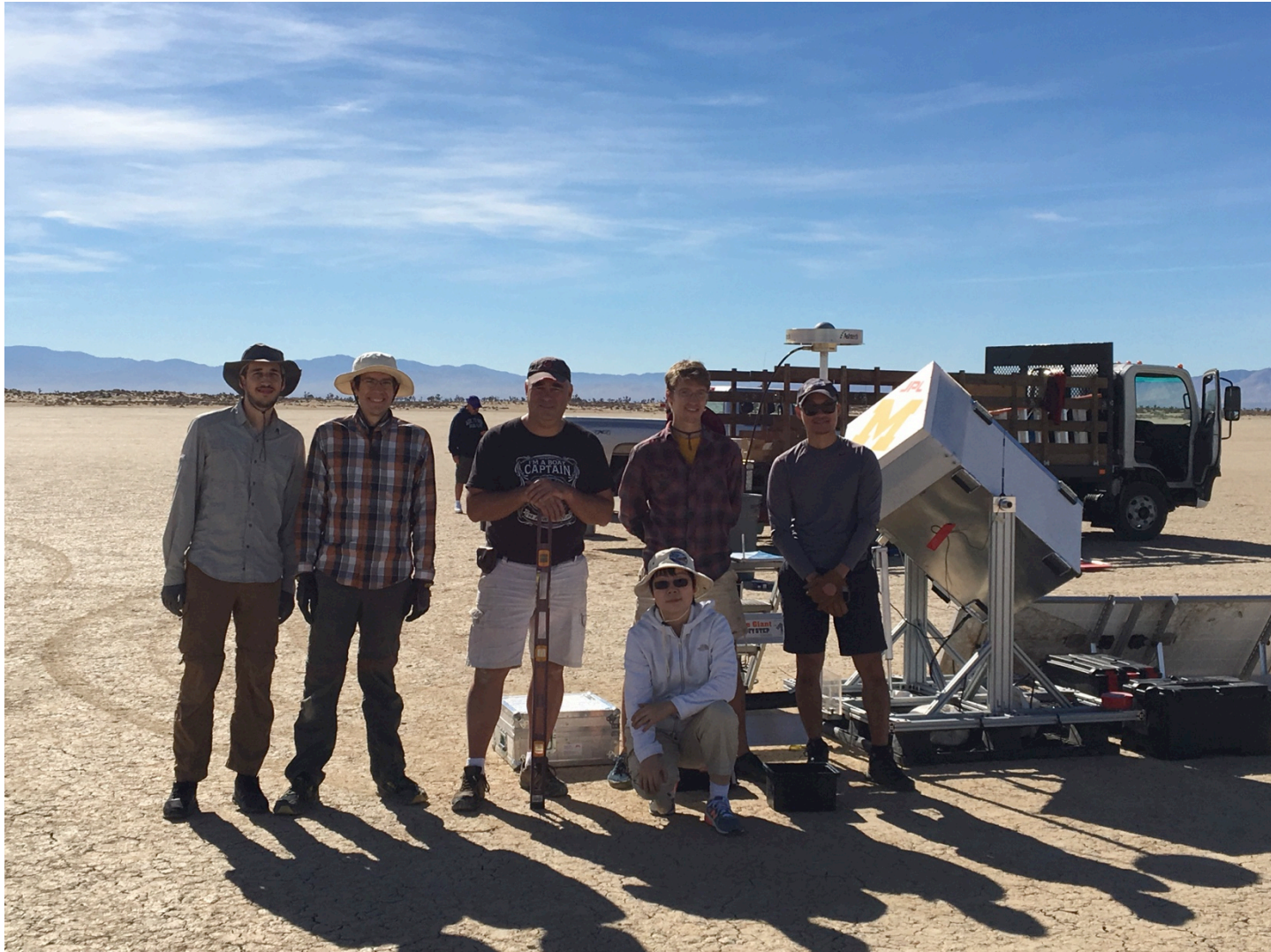
NISAR and UAVSAR Clutter Statistics

UAVSAR/ NISAR power characteristics		
	UAVSAR	NISAR
Peak Transmit Power	3.1 kW	1.2 kW
Antenna Gain	18.9 dBi	34.8 dBi
Operation Altitude	12.5 Km	600 Km
Look Angle (deg)	15-60	30-41
PARC Received Power	-19dBm	-41dBm
PARC active gain	37 dB	52 dB
PARC transmit power	18 dBm	11 dBm

PARC SPECS		
	UAVSAR	NISAR
Frequency Range	1217.5 -1317.5MHz	
Bandwidth	100 MHz	
Antenna Gain	16.5 dBi	
Active Gain	37dB	52dB
RCS	40 dBsm	55 dBsm
Worse Case Signal to Clutter ratio	43.7 dB	34.9 dB
Max power	<20dBm (0.1 Watt)	

First Installed November 1, 2018

And UAVSAR Flight and Data Collect November 7, 2018



Compute PARC RCS from Standard Calibration

Backscatter SAR assumes reciprocity such that $S_{hv} = S_{vh}$
results in calibration coefficients as such:

$$\Sigma_{HH} = \frac{1}{A} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(HH)_{observed}}}$$

$$\Sigma_{HV} = \frac{1}{Afg} = \frac{\sqrt{\Sigma_{HH}} \sqrt{\Sigma_{VV}}}{\left(\frac{\sqrt{\langle S_{VH} S_{VH}^* \rangle}}{\left(\sqrt{\langle S_{HV} S_{HV}^* \rangle} \right)^{\frac{1}{2}}} \right)^{\frac{1}{2}}}$$

$$\Sigma_{VH} = \frac{g}{Af} = \frac{\sqrt{\Sigma_{HH}} \sqrt{\Sigma_{VV}}}{\left(\frac{\sqrt{\langle S_{HV} S_{HV}^* \rangle}}{\left(\sqrt{\langle S_{VH} S_{VH}^* \rangle} \right)^{\frac{1}{2}}} \right)^{\frac{1}{2}}}$$

$$\Sigma_{VV} = \frac{1}{Af^2} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(VV)_{observed}}}$$

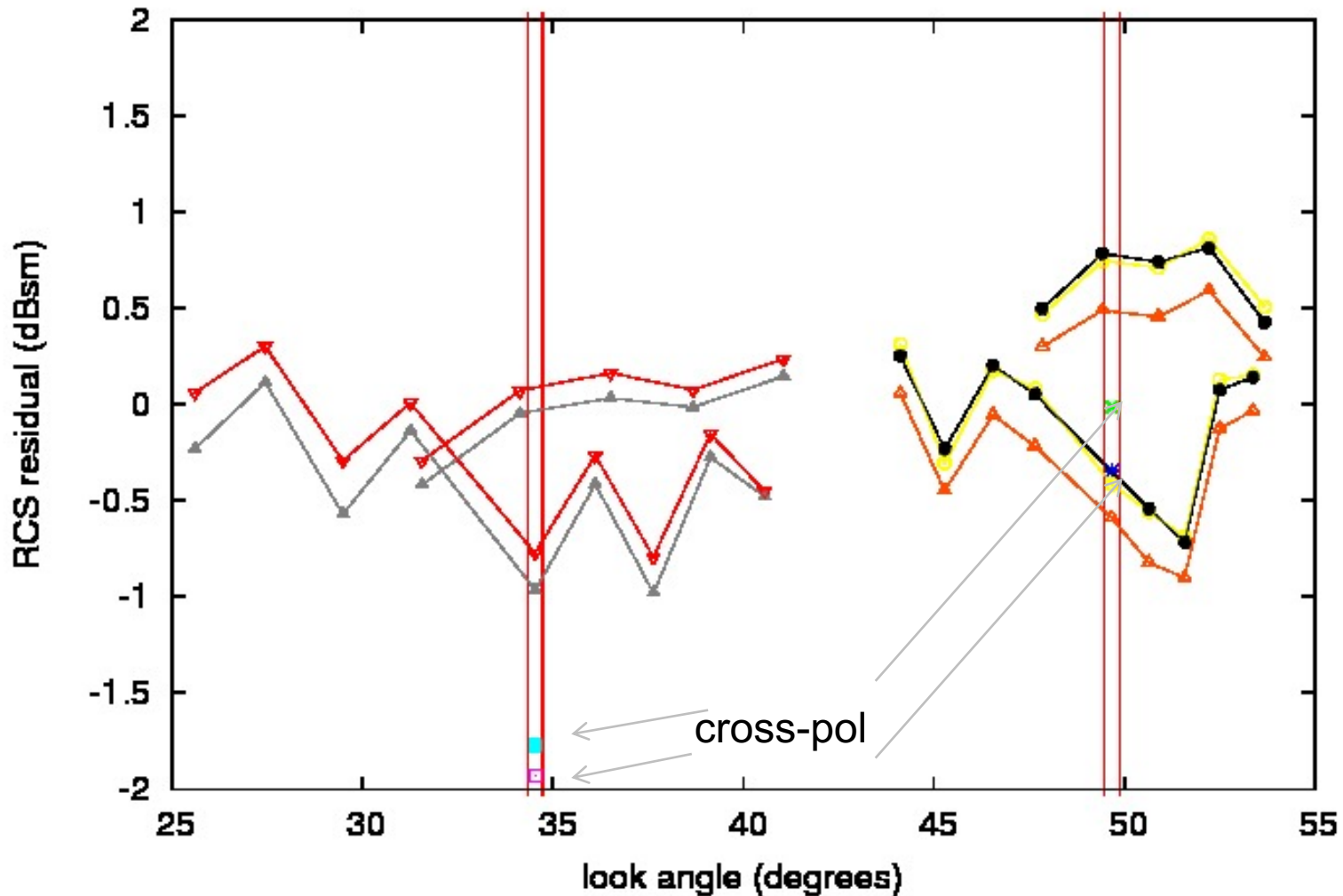
where $A^2 = \frac{\langle S_{HH} S_{HH}^* \rangle}{\sigma_{cr}}$ and $f^4 = \frac{\langle S_{VV} S_{VV}^* \rangle}{\langle S_{HH} S_{HH}^* \rangle}$ are computed at the CR

$g^4 = \frac{\langle S_{HV} S_{HV}^* \rangle}{\langle S_{VH} S_{VH}^* \rangle}$ is computed within the image

PARC and CR RCS Comparison

Five 350 Degree Heading Data Lines over RCRA with cross-pol channel imbalance = 1.2912

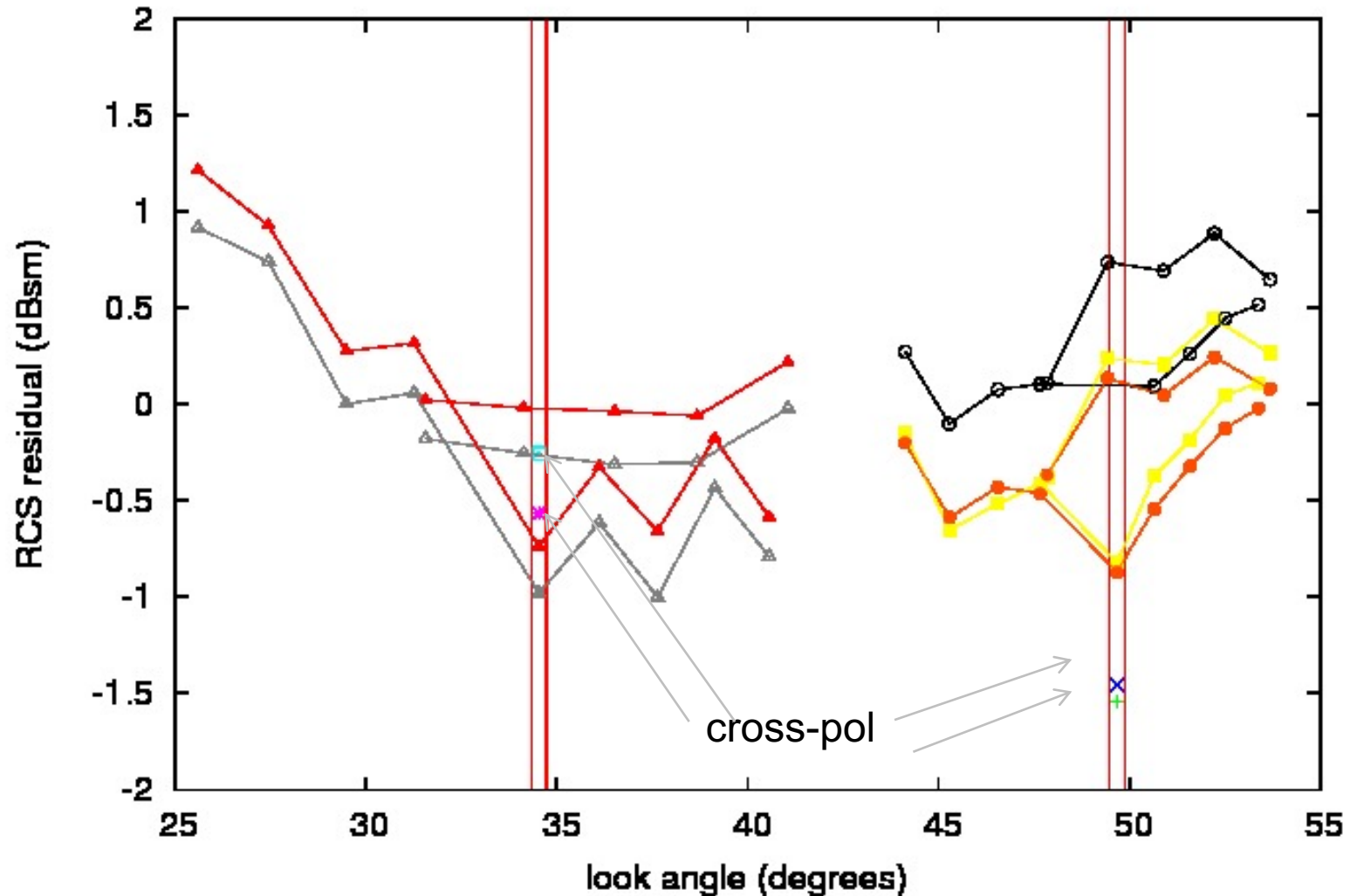
07 Nov 2018 data flight, HH and HV RCS residuals



PARC and CR RCS Comparison

Five 350 Degree Heading Data Lines over RCRA with cross-pol channel imbalance = 1.2912

07 Nov 2018 data flight, VV and VH RCS residuals

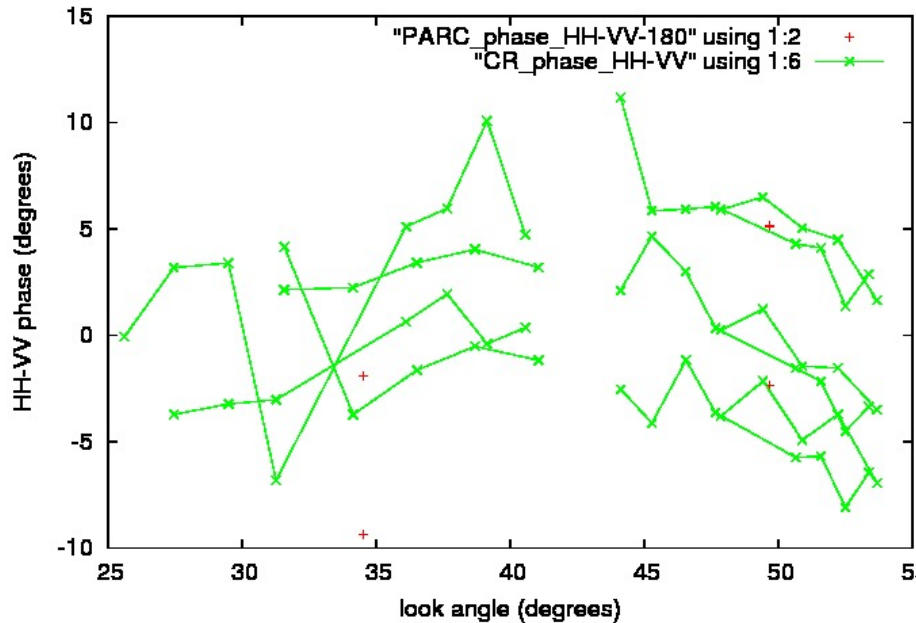


PARC Phase Comparison

Five 350 Degree Heading Data Lines over RCRA

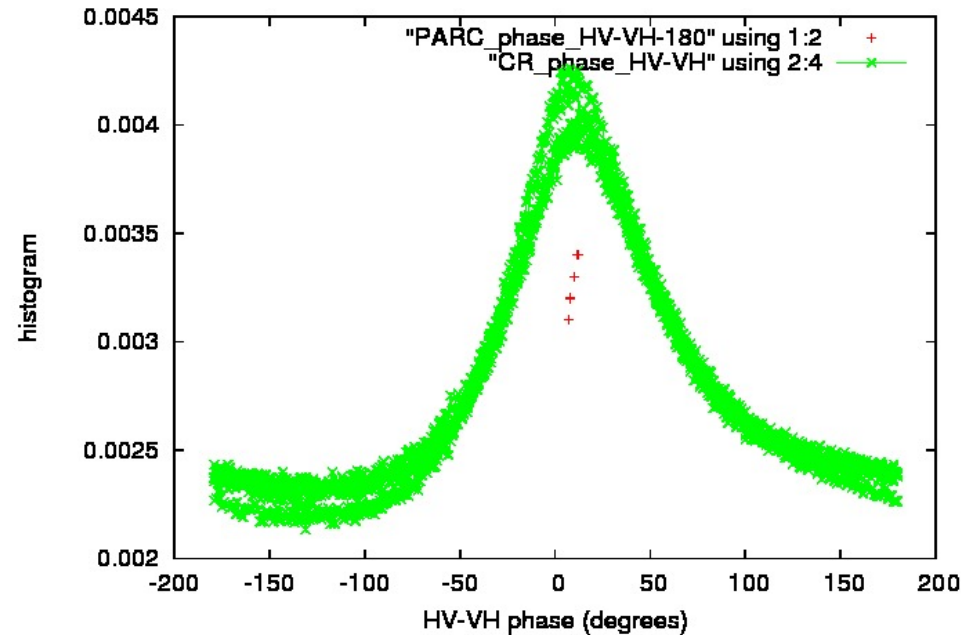
For PARC, recall that: $\phi_{HH-VV} = \phi_{HV-VH} = \pi$

07 Nov 2018 flight, HH-VV phase



ϕ_{HH-VV} is computed
at the CR

07 Nov 2018 flight, HV-VH phase histogram and PARC



$\arg (\langle S_{HV}, S_{VH}^* \rangle)$ is computed
within the image

Using the PARC for Calibration of the Cross-Pol Channel Imbalance

$$\Sigma_{HH} = \frac{1}{A} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(HH)_{observed}}}$$

$$\Sigma_{HV} = \frac{1}{Afg} = \sqrt{\Sigma_{HH}} \sqrt{\Sigma_{VV}} \frac{(\sqrt{\langle S_{VH} S_{VH}^* \rangle})^{\frac{1}{2}}}{(\sqrt{\langle S_{HV} S_{HV}^* \rangle})^{\frac{1}{2}}}$$

$$\Sigma_{VH} = \frac{g}{Af} = \sqrt{\Sigma_{HH}} \sqrt{\Sigma_{VV}} \frac{(\sqrt{\langle S_{HV} S_{HV}^* \rangle})^{\frac{1}{2}}}{(\sqrt{\langle S_{VH} S_{VH}^* \rangle})^{\frac{1}{2}}}$$

$$\Sigma_{VV} = \frac{1}{Af^2} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(VV)_{observed}}}$$

where $A^2 = \frac{\langle S_{HH} S_{HH}^* \rangle}{\sigma_{cr}}$ and $f^4 = \frac{\langle S_{VV} S_{VV}^* \rangle}{\langle S_{HH} S_{HH}^* \rangle}$ are computed at the CR

but now $g^4 = \frac{\langle S_{HV} S_{HV}^* \rangle}{\langle S_{VH} S_{VH}^* \rangle}$ is computed by the PARC at the CR

Using the PARC for Calibration of the Cross-Pol Channel Imbalance

	from image	from PARC	Look Ang.
Rosamd_35012_000	1.3414	1.4100	49.7
Rosamd_35017_001	1.3085	1.1938	34.5
Rosamd_35012_013	1.3404	no value	
Rosamd_35017_014	1.2503	1.1828	34.5
Rosamd_35012_017	1.2154	1.3766	49.7
Average	1.2912	1.2908	

Using the PARC for Calibration

Computation of Cross-Pol calibration coefficients from PARC

$$\Sigma_{HH} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(HH)_{observed}}}$$

$$\Sigma_{HV} = \frac{Equivalent_PARC_RCS_Setting}{\sqrt{RCS(HV)_{observed}}}$$

$$\Sigma_{VH} = \frac{Equivalent_PARC_RCS_Setting}{\sqrt{RCS(VH)_{observed}}}$$

$$\Sigma_{VV} = \frac{\sqrt{\sigma_{cr}}}{\sqrt{RCS(VV)_{observed}}}$$

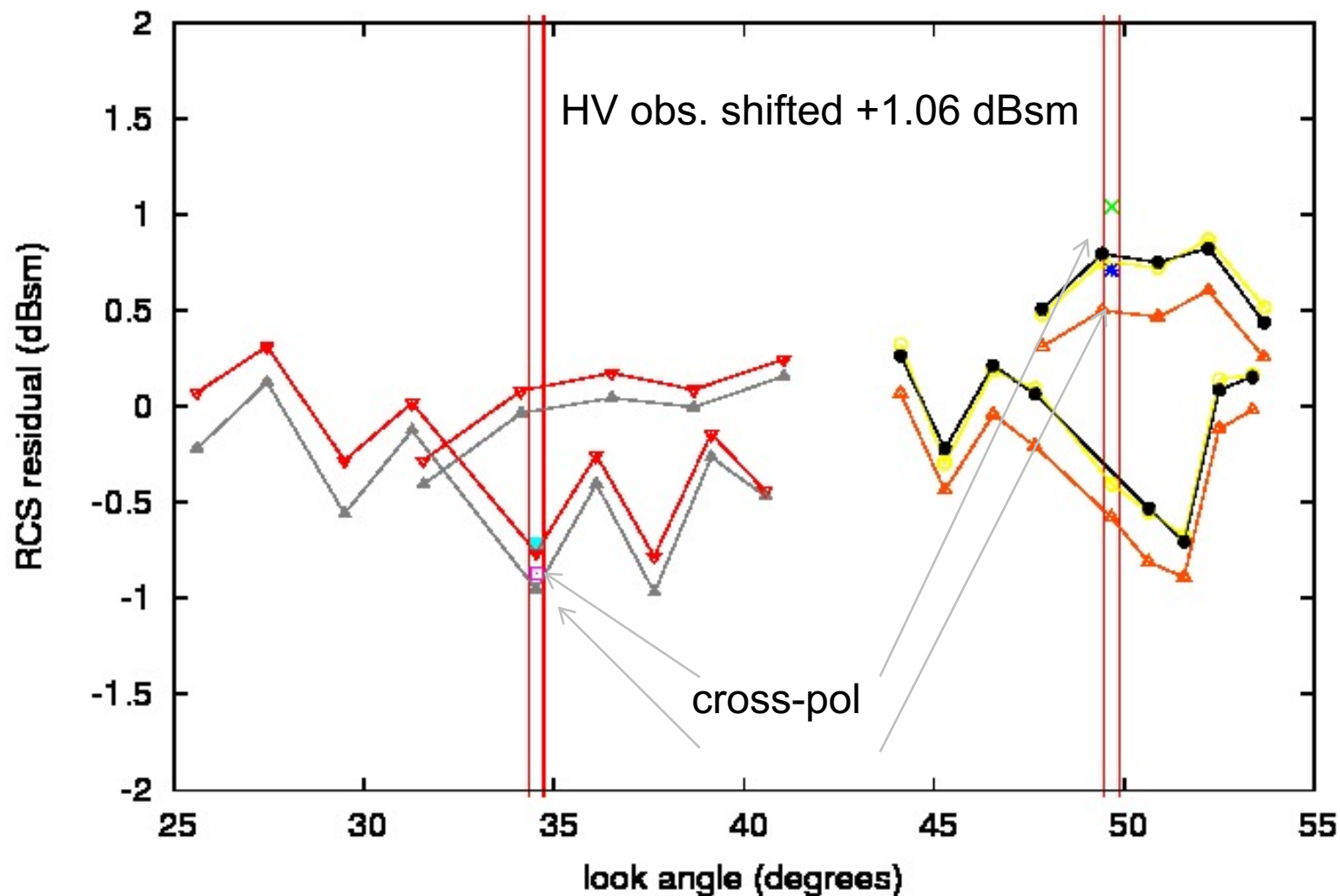
where co – channel imbalance $f^4 = \frac{\langle S_{VV} S_{VV}^* \rangle}{\langle S_{HH} S_{HH}^* \rangle} = \frac{\Sigma_{HH}^2}{\Sigma_{VV}^2}$

and cross – channel imbalance $g^4 = \frac{\langle S_{HV} S_{HV}^* \rangle}{\langle S_{VH} S_{VH}^* \rangle} = \frac{\Sigma_{VH}^2}{\Sigma_{HV}^2}$

PARC and CR RCS Comparison

Five 350 Degree Heading Data Lines over RCRA
with effective cross-pol channel imbalance = 1.2850 (was 1.2912)

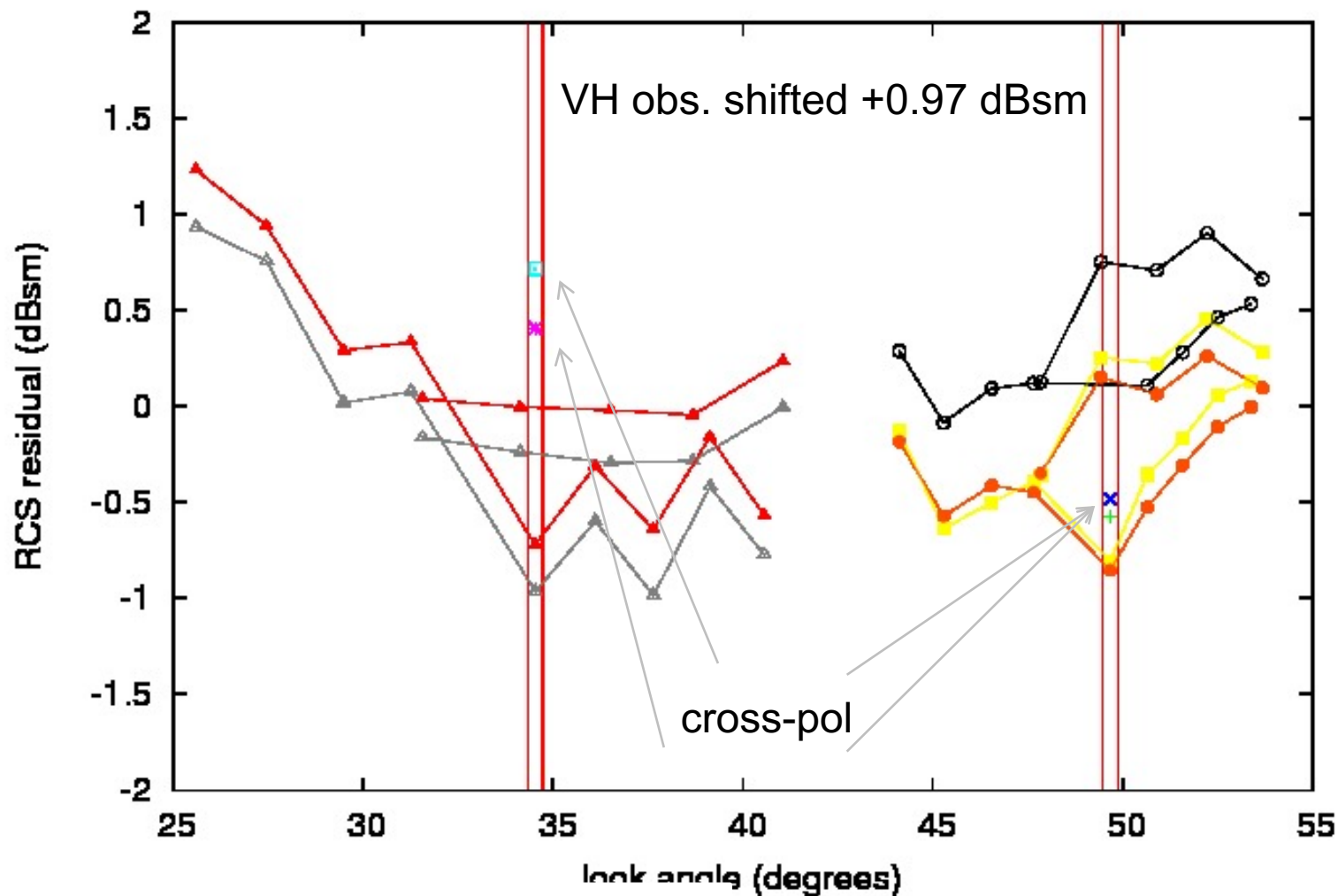
07 Nov 2018 data flight, HH and HV RCS residuals



PARC and CR RCS Comparison

Five 350 Degree Heading Data Lines over RCRA
with effective cross-pol channel imbalance = 1.2850 (was 1.2912)

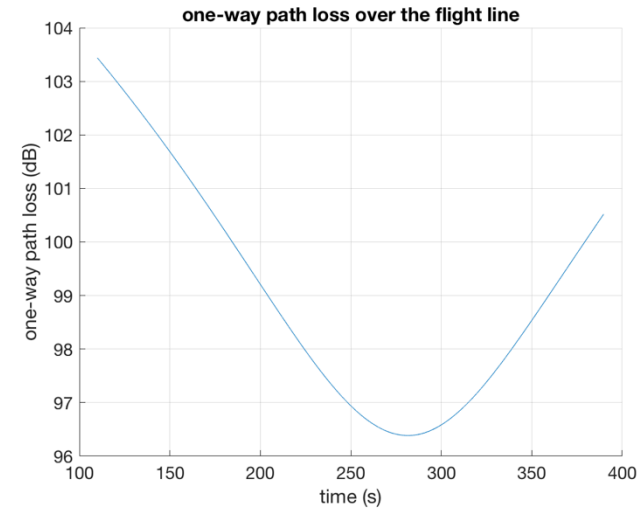
07 Nov 2018 data flight, VV and VH RCS residuals



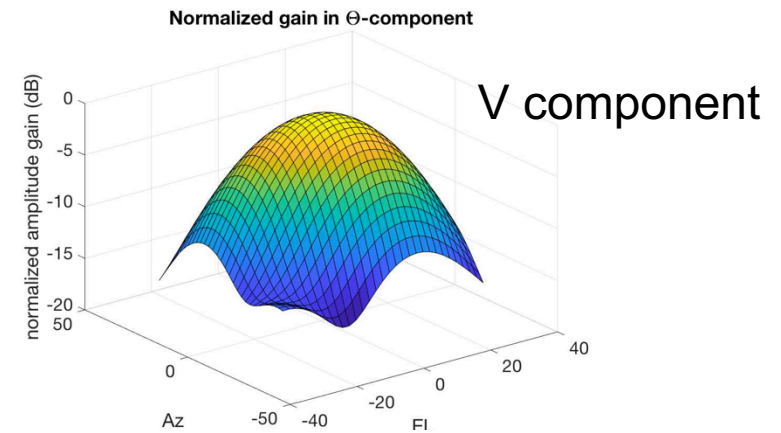
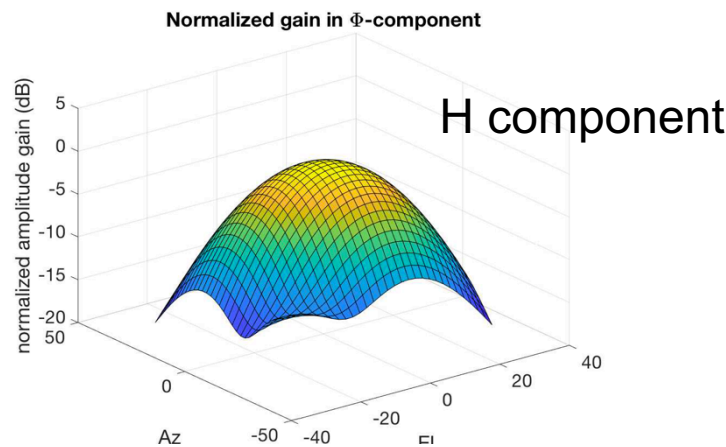
Observing the Platform Antenna Pattern

Account for one-way path loss

$$PathLoss_{dB} = 20 \log_{10} Range$$



Account for PARC antenna pattern of 45 degree rotated horn antenna

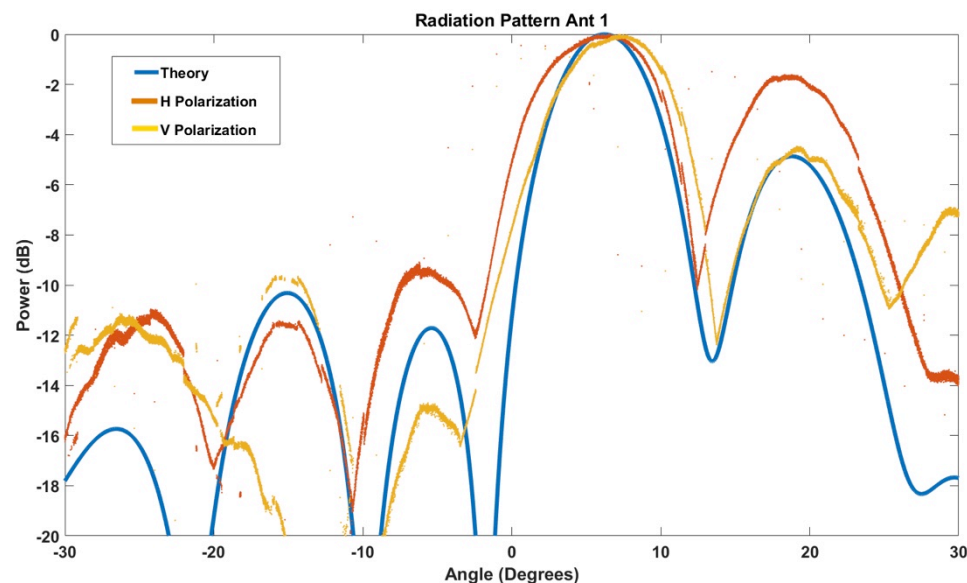
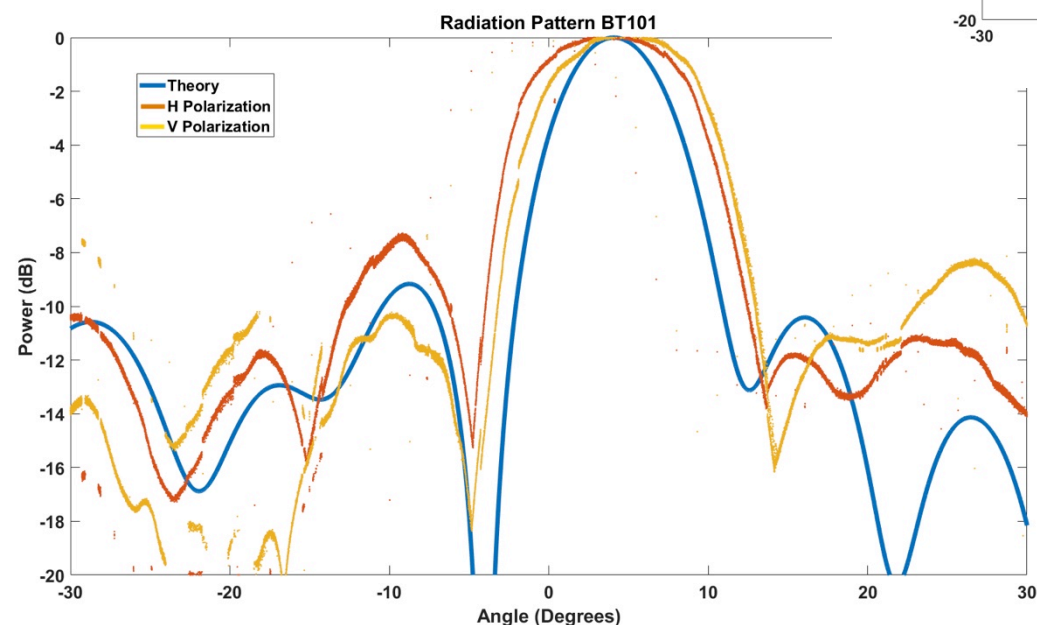


$$ParcAntGain_{H,dB} = 13.5 + 20 \log_{10} |G_{\phi}(El, Az)|$$

$$ParcAntGain_{V,dB} = 13.5 + 20 \log_{10} |G_{\theta}(El, Az)|$$

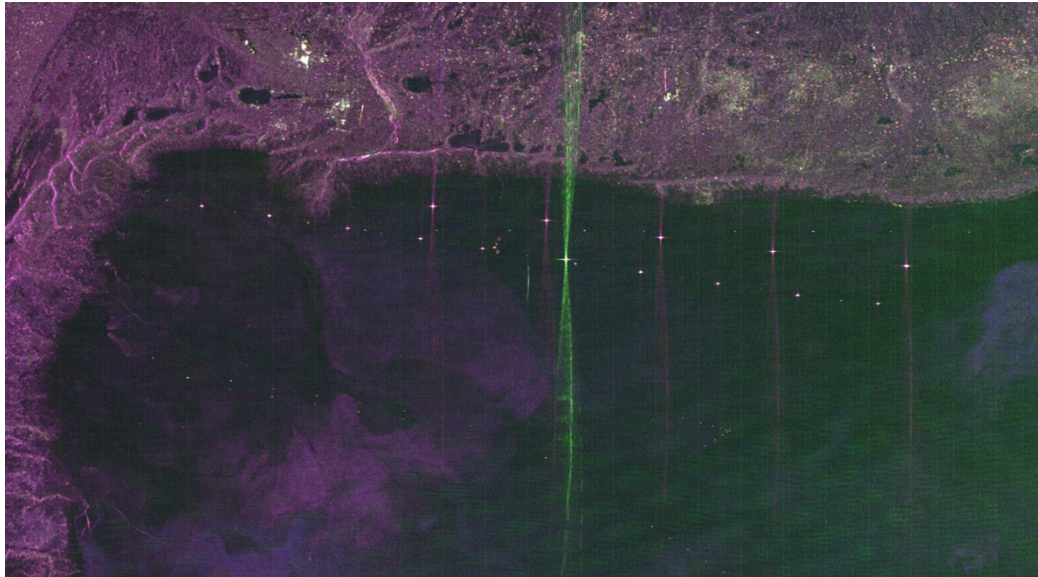
Observing the Platform Antenna Pattern

Nov 7th data flight included passes with two different antenna tables, BT101 and Ant 1.



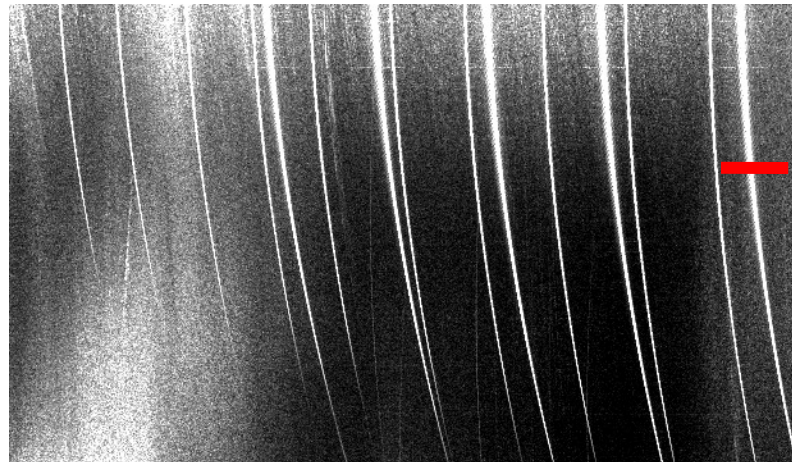
The predicted model computed from Beam Table Generator code using ~10Y old TR module measurement responses.

Phase Tracking the Peak Magnitude of Range Compressed Data Provides Relative Range Error of Platform

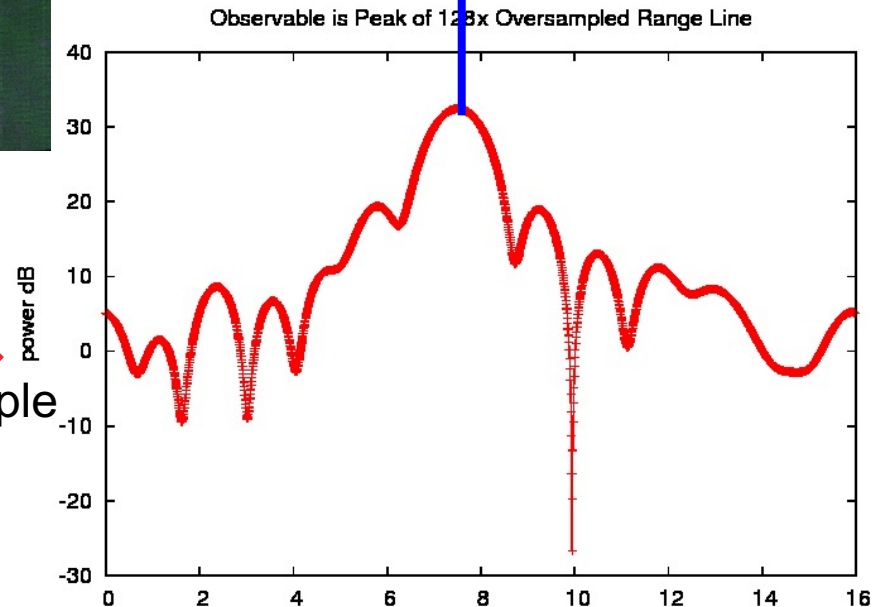


$$\delta r = f(\text{corner}, \text{platform}, \text{trop})$$

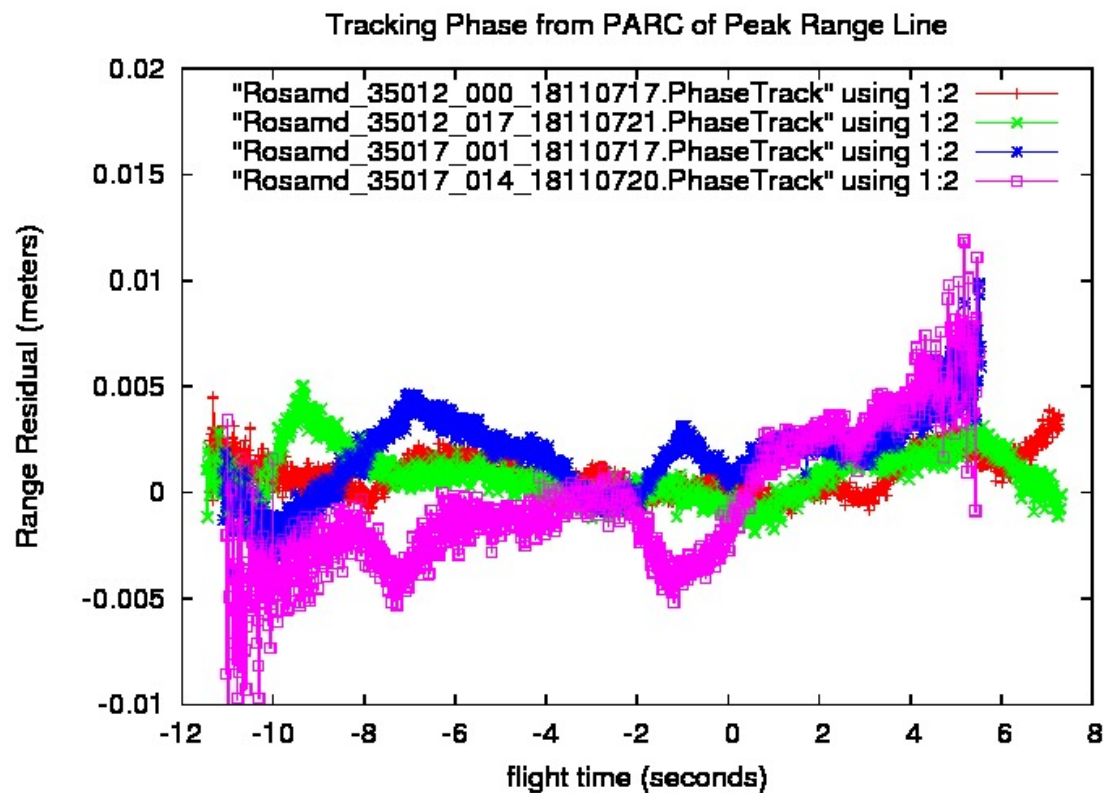
$$\varphi = \arg\left(S_{\max} \times e^{\frac{4\pi i \delta r}{\lambda}}\right)$$



oversample



Phase Tracking the PARC



Preliminary computations show that the phase center of the PARC is 16.8 CMS below the face of the PARC with a 26.6 nsec time delay.

Data Line	PARC Setting	Look Angle	Range Error RMS
35012_000 (mid)	45 dBsm	49.7 degrees	1.2 mm
35012_017 (mid)	45 dBsm	49.7 degrees	1.4 mm
35017_001 (near)	45 dBsm	34.5 degrees	2.5 mm
35017_014 (near)	40 dBsm	34.5 degrees	3.2 mm

Summary

- University of Michigan has delivered to UAVSAR-- a JPL/NASA institutional instrument-- a Single Antenna Polarimetric Active Radar Calibrator.
 - Second PARC to be delivered in 2019.
- First data acquired from the PARC was from UAVSAR on November 7th, 2018
- Good Co-Pol and RCS agreement with Trihedral Corners at RCRA.
 - Possible ~ 1dBsm look-angle dependent Cross-Pol (very preliminary).
- Good HH-VV phase agreement with CRs.
- Very good HV-VH phase agreement with background.
- Amplitude data from PARC ground acquisitions agrees with predicted UAVSAR transmit antenna pattern.
 - Goal is to prepare an optimum antenna table for existing L-band Antenna.
- Phase tracking the PARC return at 45 dBsm shows several mm of platform (UAVSAR) range error over 20 seconds.
 - Expectation is to increase PARC RCS to 55 dBsm to acquire 40 seconds (at least 2 patches) of L-band data to aid in tuning the platform metrology stochastic modeling.
- Need to investigate effect of ~27 nsec PARC time delay and the effect on SAR focusing and RCS.



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